



自适应聚焦下基于强度传输方程的相位恢复

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Phase retrieval based on the transport of intensity equation under adaptive focus

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Abstract: The non-interference phase retrieval method based on the transport of intensity equation was a method to obtain the phase by solving the intensity images. In the process of image acquisition, the selection of in-focus image was very important. But it was usually determined by subjective methods, which led to inaccurate in-focus positioning, thus affecting the accuracy of phase results. Firstly, an phase retrieval method based on the transport of intensity equation under adaptive focus was proposed; Secondly, the edge duty ratio was used to locate the acquired images in this algorithm. After solving the phase, the optimal focus position was located when the edge duty ratio locating position kept unchanging by the circular angular spectrum propagation; Finally, the phase of the sample was solved by using the transport of intensity equation. The result show that this algorithm not only improved the accuracy of phase retrieval, but also reduced the time to obtain a large number of images. In the simulation experiment, the correlation coefficient between the retrieval phase and the original phase reached 0.9866, and the RMSE error is 0.3050. In the actual experiment of microlens array, the error between the true height of the microlens and the height solves by the phase retrieval method proposed is only 5.7%, which proves that the algorithm can locate the optimal focus position in the field of microscopic imaging. And the algorithm is conducive to the development of auto-focus technology and improves the accuracy of phase retrieval.

Key words: phase retrieval; transport of intensity equation; adaptive focus; edge duty ratio

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自适应聚焦下基于强度传输方程的相位恢复

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摘 要:基于强度传输方程的非干涉相位恢复方法是通过对强度图像求解方程来获取相位的一种途径。在图像采集过程中,对聚焦图像的选择是很重要的。但该过程通常是由主观方法来确定,从而导致聚焦定位不准确,进而影响相位恢复结果的精度。首先,提出了一种基于强度传输方程的自适应聚焦相位恢复方法;其次,使用边缘占空比对采集图像进行定位,在求解相位之后进行循环角谱传播,直到边缘占空比定位位置不变,即被认为是定位到了最佳聚焦位置;最后,再使用强度传输方程求解样本的相位。结果证明:该方法不仅提高了相位恢复的准确性而且减少了获取大量图像的次数。在模拟实验中,恢复相位与原始相位的相关系数达到 0.9866,均方根误差为 0.3050。在实际的微透镜阵列实验

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中,用所提出的相位恢复方法恢复出的微透镜高度与真实高度误差仅为 5.7%,证明了在显微成像领域,所提算法可以定位到最优聚焦位置,有利于自动聚焦技术的发展,进而提高相位恢复的精度。 关键词:相位恢复; 强度传输方程; 自适应聚焦; 边缘占空比

0 Introduction

In the field of optical microscopy, phase research provides information such as depth and refractive index for biological cells and other objects, which has become an important reference index. At the same time, the solution method of phase is also widely concerned. Among them, the non-interference phase retrieval method based on the Transport of Intensity Equation (TIE) has been applied to microscopic fields, such as living cell detection^[1], red blood cell detection^[2], breast cancer cell quantitative imaging^[3], etc, because it solves the equation directly through the intensity image to obtain the phase, does not need complicated calculation and devices, and reduces coherent noise^[4–6].

When solving TIE, it is necessary to obtain the focus image and the corresponding defocus images along the optical axis direction^[7-8]. In actual operation, a series of intensity images are usually obtained along the optical axis direction. But it is impossible to determine whether focus images are included in the collected images. In the case of containing the focus image, simple subjective identification can not find the optimal focus position, thus affect the accuracy of phase retrieval. In the case of not containing the focus image, it is often necessary to locate the position of the focus image through the acquisition of a large number of images again, which leads to the complicated process of phase solution. As for the positioning of microfocus images, many experts and scholars have made hardware modifications. Mao Bangfu of Zhejiang University^[9] designed a microscopic automatic focusing system. The system drives the microhandwheel of the microscope rotation through a stepping motor, which makes the stage move up and down to realize the function of automatic focusing. However, this modification requires complicated devices and high cost. Yu Yang et al. [10] of Nanjing University of Aeronautics and Astronautics have designed a microscope hardware auto-focusing system based on photoelectric position sensitive detector (PSD), which can control the displacement in the *z*-axis direction of the automatic microscope system in real time. It also improves the autofocusing capability of the microscope. However, the input-output linearity of the hardware system is not accurate and needs linear compensation.

In terms of software, Tian Xiaolin et al.[11] of Jiangnan University used cell duty ratio to judge the infocus images, which judges image focus by calculating the area ratio of the sample to the background. But for continuous samples, it is impossible to distinguish between the sample and the background. So this method is only applicable to discrete samples. Cheng Hong et al.[12] of Anhui University proposed an transport of intensity equation algorithm(EDR-TIE) based the edge detection and duty ratio, which expanded the application range of samples. However, this method requires the collected image sequence to contain the focus image, and the position of the focus image is determined through onetime positioning by the algorithm. When there is no focus image in the collected image sequence, the algorithm cannot accurately locate. On this basis, this paper proposed a phase retrieval algorithm (AF-TIE) based on the transport of intensity equation under adaptive focus. This algorithm locates the reference focus position by edge duty ratio from the original image sequence, and then uses the reference focus image to calculate the focus position. It is suitable for discrete samples and continuous samples, and there is no restriction on whether the focus image is contained or not.

1 Transport of intensity equation

In a coherent light field, assuming that monochromatic light propagates along the z-axis under the 第 3 期 www.irla.cn 第 51 卷

condition of paraxial approximation. Teague deduced the transport of intensity equation^[13], which can be expressed as:

$$\left. \frac{\partial I(x, y, z)}{\partial z} \right|_{z=z_0} = -\frac{\lambda}{2\pi} \nabla \cdot (I(x, y, z_0) \nabla \phi(x, y, z_0)) \tag{1}$$

Among them, z_0 is the propagation distance, λ is wavelength, $I(x,y,z_0)$ and $\phi(x,y,z_0)$ are the intensity and phase of the object on the focus plane, $\nabla = (\partial_x, \partial_y)$ is the gradient operator on the plane of x-y, $\partial I(x,y,z)/\partial z$ represents the amount of variation in the intensity distribution along the axis, i.e. intensity differential, which cannot be measured directly and is usually estimated by using finite difference. Assuming the $I(x,y,z_0+\Delta z)$ and $I(x,y,z_0-\Delta z)$ are the over-focus intensity image and the under-focus intensity image when the defocus distance is Δz , as shown in Fig.1. The intensity differential can be zapproximately estimated by Eq.(2):

$$\left. \frac{\partial I(x,y,z)}{\partial z} \right|_{z=z_0} \approx \frac{I(x,y,z_0+\Delta z) - I(x,y,z_0-\Delta z)}{2\Delta z} \tag{2}$$

Substitute Eq.(2) into Eq.(1) can be obtained:

$$\frac{I(x, y, z_0 + \Delta z) - I(x, y, z_0 - \Delta z)}{2\Delta z} = \frac{\lambda}{2\pi} \nabla \cdot (I(x, y, z_0) \nabla \phi(x, y, z_0))$$
(3)

The only unknown quantity $\phi(x, y, z_0)$ can be obtained through Eq.(3).

In microscopic imaging, the built-in LED light wave used is partially coherent. The corresponding $\phi_{out}(x,y,z_0)$ is a generalized phase, which consists of the phase of the illumination light $\phi_{in}(x,y,z_0)$ and the phase of the object $\phi(x,y,z_0)$, i.e.

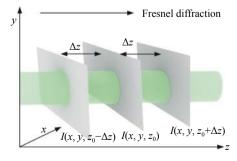


Fig.1 Schematic diagram of intensity differential estimation

$$\phi_{out}(x, y, z_0) = \phi_{in}(x, y, z_0) + \phi(x, y, z_0)$$
 (4)

Because the microscope satisfies the infinity correction optical system, i.e. the telecentric optical path. At the same time, using symmetrical Kohler illumination in the microscope, which satisfy the zero distance condition. Therefore, the phase of partially coherent light is consistent with that of traditional objects, and the corresponding generalized TIE is completely consistent with that of completely coherent illumination. Therefore, the traditional TIE phase retrieval method can be directly used to solve the phase of the object under the partially coherent light field in the microscope^[14].

2 AF-TIE algorithm

As shown in Eq.(3), the accurate selection of the focus image will affect the accuracy of phase retrieval. The edge duty ratio positioning method can help focus determination. the edge duty ratio is shown in Eq.(5)^[12]:

$$\eta = \frac{N_B}{N_T - N_B} \tag{5}$$

 N_T is the total number of pixels of the picture, N_B indicate the corresponding edge information point pixels of the object.

In this paper, the Prewitt operator is used to extract the edge information of the image. The neighborhood pixel gray value of the image function f(x,y) at point (i,j) is showed in Fig.2(a). Fig.2(b) and Fig.2(c) are the Prewitt

f(i-1,j-1)		f(i-1, j)			f(i-1,j+1)			
f(i,j-1)		f(i,j)			f(i, j+1)			
f(i+1, j-1)		f(i+1, j)		()	f(i+1, j+1)			
(a)								
	-1	-1	-1		-1	0	1	
	0	0	0		-1	0	1	
	1	1	1		-1	0	1	
		(b)	-			(c)		

Fig.2 Edge detect. (a) The gray value of the image's neighborhood pixel at (i,j); (b) Prewitt operator level template; (c) Prewitt operator vertical template

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operator template of horizontal and the vertical respectively. The gradient amplitude ∇f and first derivative g are shown in Eq.(6):

$$\begin{cases} g_x = [f(i+1,j-1) + f(i+1,j) + f(i+1,j+1)] - \\ [f(i-1,j-1) + f(i-1,j) + f(i-1,j+1)] \\ g_y = [f(i-1,j+1) + f(i,j+1) + f(i+1,j+1)] - \\ [f(i-1,j-1) + f(i,j-1) + f(i+1,j-1)] \\ \nabla f = \sqrt{g_x^2 + g_y^2} \end{cases}$$
(6)

Duty ratio as the evaluation standard of focus image, which is the area ratio of the sample to the background in the image actually. When the collected intensity map is located in the focused plane, the target sample occupies the least area in the image. If the position deviates from the focal plane, halos will appear under the influence of diffraction effect, blurring the sample boundary, thus increasing the proportion of sample edge information in the whole image area. With the increase of defocus distance, the proportion of edge information will be larger. Therefore, the focus intensity image can be judged by calculating the number of pixels occupied by the sample edge, that is to say the focus position can be located from a series of intensity maps by using the characteristic of "the duty ratio of the optimal focus image is the minimum"^[9].

When the collected image sequence contains focus image, the EDR-TIE algorithm proposed in reference[12] can be used directly to detect the optimal focused position. However, when the focus image is not included, use the EDR-TIE algorithm directly can only be used to locate in the first or the last position of this column of intensity images. So, in order to obtain the focus position, we need to collect a large number of images again. Based on EDR-TIE, this paper proposes an positioning method of adaptive focusing, i.e. AF-TIE algorithm, and its flow chart is shown in Fig.3.

Firstly, the edge duty ratio method is used to locate k_1 position through a series of existing intensity images, and the phase at k_1 position can be solved by TIE, which used intensity image and corresponding defocus images.

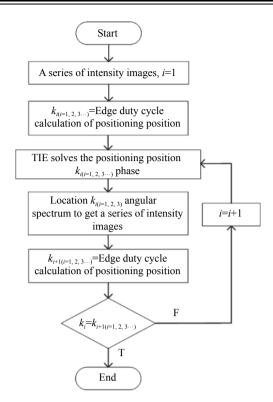


Fig.3 Algorithm flow chart

The phase and intensity form a wavefront. Then use the angular spectrum propagation to obtain a new series of intensity images. The edge duty ratio is used to detect and locate, and the position is found to be k_2 . If k_1 and k_2 are equal, k_1 is considered to be the optimal focus position, and the focus image are considered to be contained in the series of intensity maps. If k_1 and k_2 are not equal, the intensity image and the corresponding defocus images of k_2 position are obtained. So the phase of k_2 position is solved, and a new series of intensity images are obtained by angular spectrum propagation again. Continue to postion with edge duty cycle, compare and cycle until the position obtained by positioning is no longer changed, ending the cycle.

In the above angular spectrum propagation, we all choose one-direction propagation, because if the collected series of intensity images contain focus image, as shown in Fig.4(b). The positioning position does not change after the first positioning and the angular spectrum propagation in one direction. If the focus image is not included, this series of intensity images can only be on the under-focus

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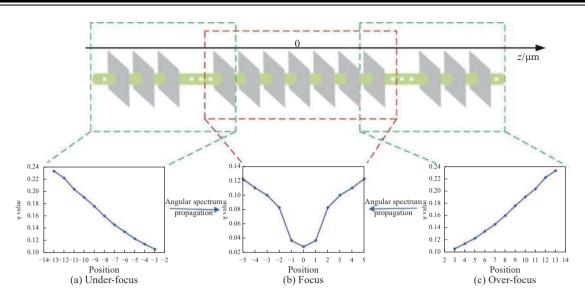


Fig.4 Schematic diagram of edge duty ratio and angular spectrum propagation direction under different conditions

side or on the over-focus side, as shown in Fig.4(a) and Fig.4(c). After the edge duty ratio is positioned. We choose to propagate the angular spectrum to the side with small edge duty ratio, that is, to the side with focus.

Assuming that the optimal focus position is at z_0' , then the defocus image $I(x,y,z_0'+\Delta z)$ and $I(x,y,z_0'-\Delta z)$ are selected at the position $z_0'\pm\Delta z$, and the Eq.(2) is used to obtain the following formula

$$\frac{\partial I(x, y, z_0')}{\partial z} \approx \frac{I(x, y, z_0' + \Delta z) - I(x, y, z_0' - \Delta z)}{2\Delta z}$$
(7)

Allen et al. proposed that the solution of Eq.(1) can be obtained by Fourier operator step-by-step calculation. Set

$$\nabla^{2} = -\frac{\lambda}{2\pi} \frac{\partial I(x, y, z_{0}')}{\partial z}$$
 (8)

For any function f(x,y), its Fourier properties can be described as:

$$\nabla f(x,y) = ixF^{-1}f_x F[f(x,y)] + iyF^{-1}f_y F[f(x,y)]$$
 (9)

$$\nabla^2 f(x, y) = -F^{-1} (f_x^2 + f_y^2) F[f(x, y)]$$
 (10)

In the formula, x and y respectively represents the vector of x and y direction, F is Fourier transform, F^{-1} is inverse Fourier transform and (f_x, f_y) is spatial frequency coordinate. Combining Eq.(8) and Eq.(10) to obtain:

$$\varphi(x, y, z_0') = F^{-1}(f_x^2 + f_y^2) F\left[\frac{\lambda}{2\pi} \frac{\partial I(x, y, z_0')}{\partial z}\right]$$
(11)

The value of the phase is obtained by using Fourier properties again, which can be expressed as:

$$\phi(x, y, z_0') = F^{-1}[(f_x^2 + f_y^2)^{-1}] \cdot F^{-1}$$

$$\{\nabla [I^{-1}(x, y, z_0') \nabla \varphi(x, y, z_0')]\}$$
(12)

3 Simulation experiment

In this section, simulation experiments are carried out on the collected image sequence with focus and without focus respectively.

3.1 Contain focus images

Firstly, the simulated experimental samples are selected. The intensity and phase images of the focus plane are shown in Fig.5(a) and Fig.5(b) respectively. The simulated image size is set to 256×256 pixel. Setting the focus position to 0 position. Firstly, five defocus images are obtained respectively before and after the focus plane by angular spectrum propagation, as shown in Fig.5(c). EDR-TIE algorithm is used directly for 11 intensity images which include focus image. The edge duty ratio detection results are shown in Fig.5(d), and it can be found that the focus image located at 0 position. The phase solution is carried out by the intensity image and the corresponding defocus images where the 0 position is located, and the result is shown in Fig.5(d).

The cycle operations continue to carry out by the

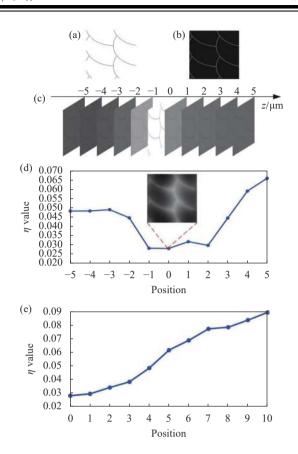


Fig.5 Simulation experiment. (a) Set intensity image; (b) Set phase image; (c) A series of intensity images (including focus) of angular spectrum propagation; (d) EDR-TIE positioning calculation results and 0 position phase results graph; (e) AF-TIE positioning calculation result graph

AF-TIE algorithm. Using the intensity image of the 0 position and the phase image obtained by the solution to do angular spectrum propagate to the in-focus side, thus 11 intensity images are obtained, then the edge duty ratio detection is carried out again. If it found that the position is consistent with which obtain by EDR-TIE algorithm, as shown in Fig.5(e). Therefore, the 0 postion is considered as the optimal focus position which matches the set focus position.

Assuming that the original phase is ϕ , the retrieved phase is ϕ_r . Define error formula as^[15]:

$$RMSE = \sqrt{\frac{\sum_{x,y} (\phi_r - \phi)^2}{M \times N}}$$
 (13)

The error of the phase result between the optimal focus position and the set position is 0.3050. It can be

seemed that both EDR-TIE and AF-TIE algorithm proposed in this paper can locate the optimal focus position when the focus image is included.

3.2 Does not contain focus image

The intensity and phase in the focus plane of the simulated experimental sample are shown in Fig.6(a) and Fig.6(b) respectively. The distance between the two adjacent images is $100 \mu m$, 0 position is the real focus position, and defocus images at positions from -8 to -13

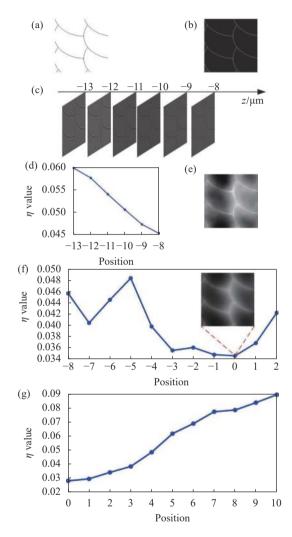


Fig.6 Simulates experiment. (a) Set intensity image; (b) Set phase image; (c) A series of intensity images (unfocused) of angular spectrum propagation; (d) EDR-TIE positioning calculation results; (e) Phase retrieval results of EDR-TIE positioning positions; (f) AF-TIE positioning calculation results and phase retrieval results; (g) A series of intensity image AF-TIE positioning calculation results propagated by the 0 position angular spectrum in Fig.6(f)

are obtained by angular spectrum propagation, as shown in Fig.6(c). There is no focus image in this series of images. EDR-TIE algorithm is directly calculated from these 6 images. The positioning result is shown in Fig.6(d), and it can be found that it is located at the position of -8. We use angle spectrum by images at -8 position to obtain the intensity at -7 position. Then, using the intensity images at positions -9, -8, and -7 to obtain the phase of -8 position through TIE and the result is shown in Fig.6(e). Obviously, the EDR-TIE positioning result is inaccurate. If we want to obtain the focus image further, we usually need to collect a large number of intensity images again. Using AF-TIE algorithm in this paper, unidirectional angular spectrum propagation and edge duty ratio detection are carried out from the intensity image and the phase image at -8 position obtained by solution, and it is found that the focus plane is located at 0 position. The result is shown in Fig.6(f). Then move the translation table to collect the intensity image and the corresponding defocus images in 0 position, and the phase result show in Fig.6(f). Once again, one-directon angular

spectrum propagation and edge duty ratio calculation are carried out to obtain the result in Fig.6(g), and it is found that it is located at its own position. Therefore, the 0 position is the optimal focus position, which is also the preseted. Then ending the cycle. This process reduce the collection number of intensity images.

In order to further compare the phase results of EDR-TIE algorithm and AF-TIE algorithm, an image quality evaluation index SSIM (structural similarity index) is introduced to measure the image structural similarity^[16].

$$SSIM(X,Y) = \frac{(2\mu_X\mu_Y + C_1)(\sigma_{XY} + C_2)}{(\mu_Y^2 + \mu_Y^2 + C_1)(\sigma_Y^2 + \sigma_Y^2 + C_2)}$$
(14)

With the two images X and Y entered, μ_X and μ_Y represent the average of X and Y, σ_X and σ_Y represent the standard deviation of X and Y, σ_{XY} is the covariance of X and Y, C_1 and C_2 are the constants.

The error and similarity between the phase results of EDR-TIE algorithm and AF-TIE algorithm and the set phase are calculated by Eq.(13) and Eq.(14) respectively, as shown in Tab.1. The effectiveness and accuracy of the algorithm proposed in this paper are proved.

Tab.1	Evaluation	results	of different	algorithms
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Algorithm evaluation index	RMSE	SSIM
EDR-TIE	0.4690	0.9687
AF-TIE	0.3050	0.9866

4 Real experiment

In this section, real experiments are carried out on samples of continuous distribution and discrete distribution respectively. A small amount of intensity images are collected by inverted microscope (MI52, Mshot), and the acquisition interval of adjacent intensity images is 2 μ m. The experimental device and internal optical path are shown in Fig.7. The illumination light source is the LED white light in the microscope. Firstly, it passes through a optical filter with a center wavelength of 532 nm and half-peak bandwidth of 22 nm. Then the light intensity adjusted by a light collector and an aperture

diaphragm. Next, we obtain uniform collimated light through a light collector. The light irradiates the sample

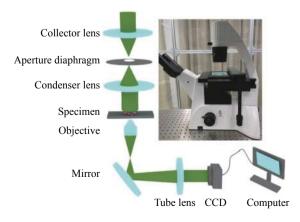


Fig.7 Experimental device diagram and internal optical path

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through the objective lens, the reflector and the lens barrel lens. Finally, the enlarged object light field is transmited to the camera port of the microscope. The resolution of CCD (MS60, Mshot) used in the experiment is $2\,048\times2\,048$ pixel.

4.1 Real experiment of continuous samples

The continuous distributed cross-cutting cells of plant rhizomes are selected as sample in the real experiment of continuous distributed samples. EDR-TIE algorithm is used to locate the collected intensity images. The results are shown in Fig.8(a), and the positioning results are ideally located at the head or tail of a series of images. The phase is solved by using the intensity image and the corresponding defocus images of EDR-TIE positioning position, as shown in Fig.8(b). 10 intensity images are obtained from the EDR-TIE positioning position through angle spectrum propagated, since a new series of intensity images are obtained. Then AF-TIE calculation and edge duty ratio positioning are carried out. The positioning position is shown in Fig.8(d). Move the

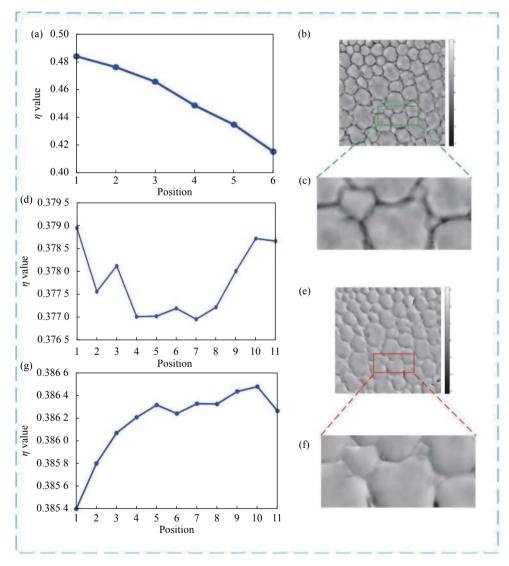


Fig.8 Real experiment-plant rhizome cross section. (a) EDR-TIE positioning calculation result diagram; (b) EDR-TIE positioning position phase result diagram; (c) Partially enlarged phase result diagram of (b); (d) AF-TIE positioning calculation result diagram; (e) AF-TIE positioning position phase result diagram; (f) Partially enlarged phase result diagram of (e); (g) Optimal focus position angle spectrum AF-TIE positioning calculation result diagram

translation table to the AF-TIE positioning position to obtain the corresponding intensity images, then solve the phase, as shown in Fig.8(e). Once again, 10 intensity images are obtained through forward angle spectrum propagation, and edge duty ratio positioning is carried out. As shown in Fig.8(g). It is found that the located position has not changed. So the cycle can be ended.

Figure8(c) and Figure8(f) are local amplification images of the phase results of Figure8(b) and Figure8(e) respectively. It can be seen that the optimal focus position can be located through several cycles by using AF-TIE algorithm.

In order to quantitatively evaluate the clarity of the retrieval phase, we use the edge duty ratio to compare the retrieval phase of EDR-TIE algorithm with AF-TIE algorithm, and the results are shown in Tab.2. It can be seen from the comparison result that when the initial image sequence does not contain focus image, the edge duty ratio of retrieval phase of the AF-TIE positioning position is smaller than the EDR-TIE positioning position, that is, AF-TIE algorithm has higher accuracy than EDR-TIE algorithm.

Tab.2 Evaluation of retrieval phase by different algorithms

Focus method	EDR-TIE	AF-TIE	
Edge duty ratio	0.142	0.138	

In order to further prove that the focus position located by AF-TIE algorithm is the optimal focus position. We move the translation stage of the microscope to the position of 7, which is the focus position located by AF-TIE algorithm, then taking 3 images at the same distance before and after the 7 position (the interval is $2 \mu m$) and directly using the edge duty ratio to locate the the optimal focus image of the 7 images. The 7 images and the positioning results are shown in Fig.9(a) and Fig.9(b). It can be seen from the results that the real shot images are also located at position 7. That is, the positioning result of the edge duty ratio on the real

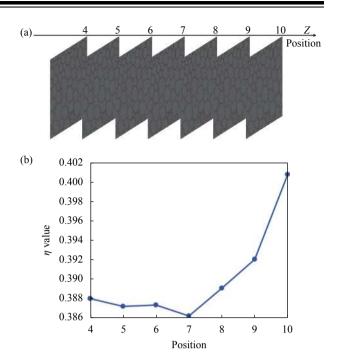


Fig.9 Validation of focused results. (a) 7 intensity images taken by the microscope; (b) Positioning result by edge duty ratio

shot image is consistent with the positioning result of AF-TIE, which proves the accuracy of the algorithm in this paper.

4.2 Real experiments of discrete samples

In this experiment, microlense (Thorlab) was choosed as sample, and the lens material was fused Shi Ying with refractive index of 1.458. EDR-TIE positioning results are shown in Fig.10(a), then solve the corresponding phase and cycle. The best focus positioning results in this paper are shown in Fig.10(b). Move the translation table to the best positioning position and capture the corresponding intensity image, then solve the phase. The phase results of the best positioning positions of EDR-TIE and AF-TIE are shown in the Fig.10(c) and Fig. 10(d) respectively. The true height of the microlens array is 1.11 um. The height of the microlens array at EDR-TIE position is 1.2805 µm with error of 15.3%. The height of the microlens array at optimal focusing position of AF-TIE is 1.1739 µm with error of 5.7%. The results show that the optimal focal plane phase height obtained by AF-TIE algorithm in this paper is closer to the real value.

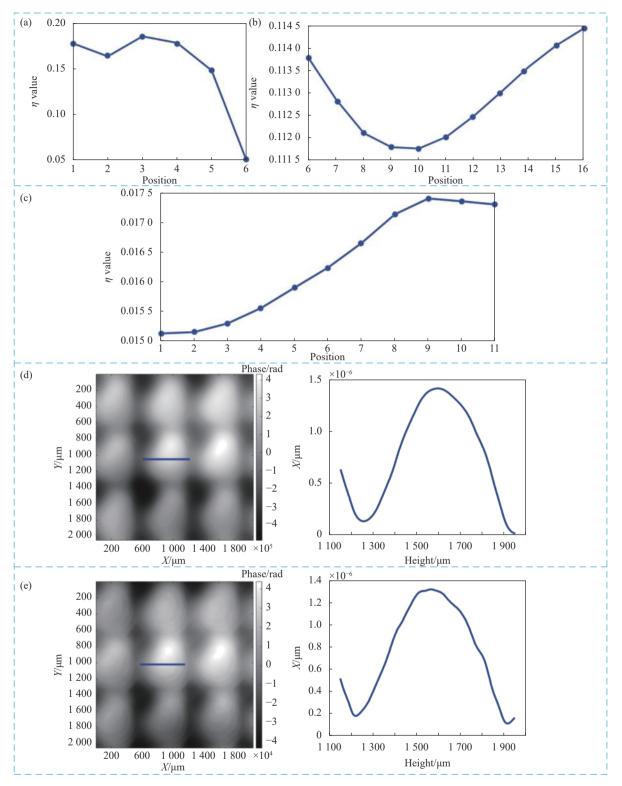


Fig.10 Actual experience micro lens array: (a) EDR-TIE positioning results; (b) AF-TIE was the best position result; (c) The optimal focus position angular spectrum AF-TIE positioning calculation result; (d) EDR-TIE position phase result and solid line section height curve; (e) AF-TIE position phase results and solid line section height curve

5 Conclusion

In the solving process of TIE, the focus image is

needed to participate. The accurate positioning of focused image is vital to improve the accuracy of phase retrieval. In the field of microscopic imaging, AF-TIE algorithm

can be used to locate the optimal focus position. For a series of images collected by microscope. Firstly, solve the phase of the first positioning position which located by the egde duty ratio. Then the circular angular spectrum propagation and focus judgment is carried out until the lacation postion remains unchanged. Where it is finally located is the optimal focus position. The AF-TIE algorithm reduce the time to obtain a large number of images, which promotes to the development of automatic focusing technology and improves the accuracy of phase retrieval.

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